



Designation: D7278 – 21

## Standard Guide for Prediction of Analyzer Sample System Lag Times<sup>1</sup>

This standard is issued under the fixed designation D7278; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

### INTRODUCTION

Lag time, as used in this guide, is the time required to transport a representative sample from the process tap to the analyzer. Sample system designs have infinite configurations so this guide gives the user guidance, based on basic design considerations, when calculating the lag time of online sample delivery systems. Lag time of the analyzer sample system is a required system characteristic when performing system validation in Practice D3764, D6122, or D8321 and in general the proper operation of any online analytical system. The guide lists the components of the system that need to be considered when determining lag time plus a means to judge the type of flow and need for multiple flushes before analysis on any sample.

### 1. Scope\*

1.1 This guide covers the application of routine calculations to estimate sample system lag time, in seconds, for gas, liquid, and mixed phase systems.

1.2 This guide considers the sources of lag time from the process sample tap, tap conditioning, sample transport, pre-analysis conditioning and analysis.

1.3 Lag times are estimated based on a prediction of flow characteristics, turbulent, non turbulent, or laminar, and the corresponding purge requirements.

1.4 Mixed phase systems prevent reliable representative sampling so system lag times should not be used to predict sample representation of a mixed phase stream.

1.5 The values stated in inch-pound units are to be regarded as standard. Other units of measurement are included in this standard and Appendix X1 examples where normally seen in industry.

1.6 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.7 *This international standard was developed in accordance with internationally recognized principles on standard-*

*ization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

### 2. Referenced Documents

2.1 *ASTM Standards:*<sup>2</sup>

D3764 Practice for Validation of the Performance of Process Stream Analyzer Systems

D6122 Practice for Validation of the Performance of Multi-variate Online, At-Line, Field and Laboratory Infrared Spectrophotometer, and Raman Spectrometer Based Analyzer Systems

D8321 Practice for Development and Validation of Multi-variate Analyses for Use in Predicting Properties of Petroleum Products, Liquid Fuels, and Lubricants based on Spectroscopic Measurements

### 3. Terminology

3.1 *Definitions:*

3.1.1 *continuous analyzer unit cycle time, n*—the time interval required to replace the volume of the analyzer measurement cell.

3.1.2 *intermittent analyzer unit cycle time, n*—the time interval between successive updates of the analyzer output.

3.1.3 *purge volume, n*—the combined volume of the full analyzer sampling and conditioning systems.

<sup>1</sup> This guide is under the jurisdiction of ASTM Committee D02 on Petroleum Products, Liquid Fuels, and Lubricants and is the direct responsibility of Subcommittee D02.25 on Performance Assessment and Validation of Process Stream Analyzer Systems.

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<sup>2</sup> For referenced ASTM standards, visit the ASTM website, [www.astm.org](http://www.astm.org), or contact ASTM Customer Service at [service@astm.org](mailto:service@astm.org). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

\*A Summary of Changes section appears at the end of this standard

3.1.4 *sample system lag time,  $n$* —the time required to transport a representative sample from the process tap to the analyzer.

3.1.4.1 *Discussion*—This includes sample conditioning unit lag time and sample loop lag time described in Practice D3764.

3.1.5 *total analyzer system response time,  $n$* —the sum of the analyzer unit response time and the analyzer sample system lag time.

### 3.2 Abbreviations:

3.2.1 *I.D.*—Internal Diameter

3.2.2 *LPM*—liters per minute

3.2.3 *SLPM*—standard liters per minute

3.2.4 *Re*—Reynolds Number

## 4. Summary

4.1 The lag time of an analyzer sample system is estimated by first determining the flow characteristics. The flow is assigned as turbulent or non-turbulent to assign the number of purges required to change out the sample. Based on the hardware employed in the sample system an estimation of the lag time can be calculated.

## 5. Significance and Use

5.1 The analyzer sample system lag time estimated by this guide can be used in conjunction with the analyzer output to aid in optimizing control of blender facilities or process units. A known and constant lag time is key for the use in optimizing control.

5.2 The lag time can be used in the tuning of control programs to set the proper optimization frequency.

5.3 The application of this guide is not for the design of a sample system but to help understand the design and to estimate the performance of existing sample systems. Additional detailed information can be found in the references provided in the section entitled Additional Reading Material.

## 6. Basic Design Considerations

6.1 *Acceptable Lag Time*—In general, a one to two minute sample system lag time should be maintained to give acceptable performance. Flow is a key component in the determination of sample system lag time, and in most systems the desired system lag time is impossible to achieve solely with maximum allowable sample flow rate to the analyzer. A fast loop or bypass can be ways to improve lag time by increasing sample velocity. A slipstream is taken from the bypass to feed the analyzer at its optimum flowrate. Excess sample in the slipstream is directed to the process stream, to flare, or vented to atmosphere, dependent upon application and regulatory requirements.

### 6.2 Physical State of Sample:

6.2.1 *Liquid Samples*—Pressure drop properties often govern the design of a liquid system. This is due for the most part on the close relationship between pressure drop and system flowrate and the fixed pressure differential available from the process for sample transport. The sizing of the sample components is a tradeoff between pressure drop and sample flowrate.

High sample flowrates in small sized component systems cause high-pressure drops and low sample transport times. The same flowrate in a larger tubing system will yield significant improvements in pressure drop through the system, but will also significantly increase the time for sample transport.

6.2.1.1 Users need to perform hydraulic calculations (which are currently outside the scope of this standard) in parallel with the lag time calculations to ensure that the “design” flow rates from a lag time perspective can actually be achieved with the operating conditions in the field with some contingency for operational variations.

6.2.2 *Vapor Samples*—Vapor phase sampling is governed less by pressure drop and more by pressure compression properties of gases relative to liquids. In compressible gases the higher the pressure in a given volume, the more sample is present in that volume. For this reason, and different from liquids, the selection and location of pressure regulating devices in the vapor sample system has a significant impact on the overall system design. The optimal location for a high-pressure regulator in a vapor sample not in a fast loop system is immediately downstream of the sample tap or high-pressure location thereby limiting the volume of the system under high pressure. Since the density of a compressible fluid is a function of the pressure, compressible fluid flow rate calculations are sometimes done over segmental lengths where average properties adequately represent the fluid conditions of the line segment. Dew point of the vapor sample must be taken into account to prevent condensation in the sample transport line.

6.2.3 *Liquid to Vapor Samples*—A change of phase due to sample vaporization can also impact the sample lag time. The volume change from the liquid phase to the vapor phase is substantial. Typical flow rates in gaseous sample lines downstream of the vaporizer not in a fast loop can represent very small liquid feed rates to the vaporizer. Deadheaded sample line lengths upstream of the vaporizer can, in turn, represent appreciable lag times.

6.2.4 *Phase Separation*—This guide is not intended to deal with dual phase samples as the volume and flow characteristics are outside the scope.

6.3 *Sample Temperature*—Temperature also impacts sample system lag time but to a lesser degree relative to pressure. Increased temperature of a sample lowers the sample density thus lowering the amount of sample flow needed to purge a given volume. Temperature impact is generally so small that it is ignored in rough estimations of sample system lag time. Temperature is paramount to prevent condensation of a vapor sample.

### 6.4 Typical Sources of Lag Time to Consider:

#### 6.4.1 Process Sample Tap:

6.4.1.1 Sample taps can be a significant source of lag time if a sampling probe is not used, need to know the design inside the sample stream. See Fig. X1.1.

6.4.1.2 Sample taps can present a problem for liquid vaporizing systems with high volume and low flow on the liquid side. See Fig. X1.2.

NOTE 1—This refers to the case where the vaporizing regulator is located at the sample tap and one then has a length of liquid filled line from the probe/process interface to the inlet of the vaporizing regulator.